

Block diagrams

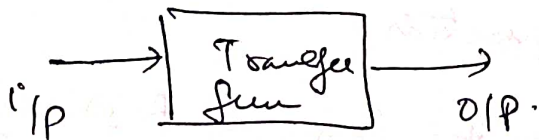
A block diagram of a system is a pictorial representation of the function performed by each component or of the flow of signals.

Such a diagram depicts the interrelationships that exists among the various components.

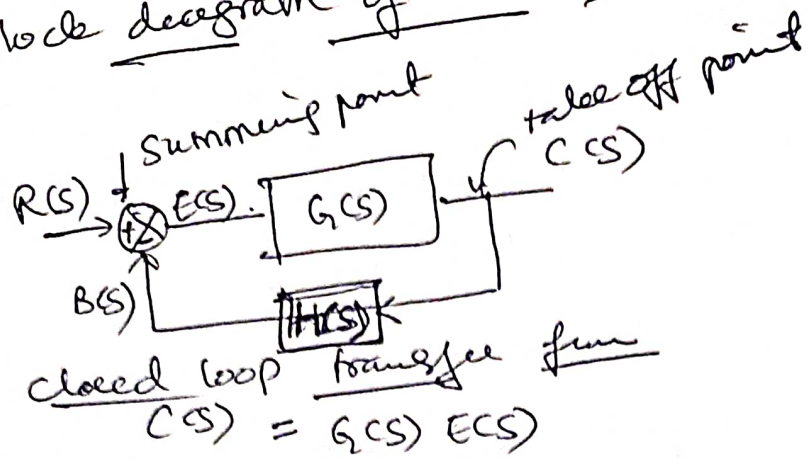
In a block diagram all system variables are linked to each other through functional blocks. Block is a symbol for mathematical operations on the input signal to the block that produces the output. The transfer fun

of the components are usually entered in the corresponding blocks which are connected by arrows to indicate the direction of flow of signals.

Eg



Block diagram of closed loop sys



$$E(s) = R(s) - B(s)$$

$$C(s) = G(s) [R(s) - B(s)]$$

$$C(s) = G(s) [R(s) - H(s) C(s)]$$

$$C(s) + H(s) C(s) = G(s) R(s)$$

$$C(s) (1 + H(s) G(s)) = G(s) R(s)$$

$$\boxed{\frac{C(s)}{R(s)} = \frac{G(s)}{1 + G(s) H(s)}}$$

or

$$\boxed{\frac{C(s)}{R(s)} = TF = \frac{G}{1 + GH}}$$

Open loop transfer function

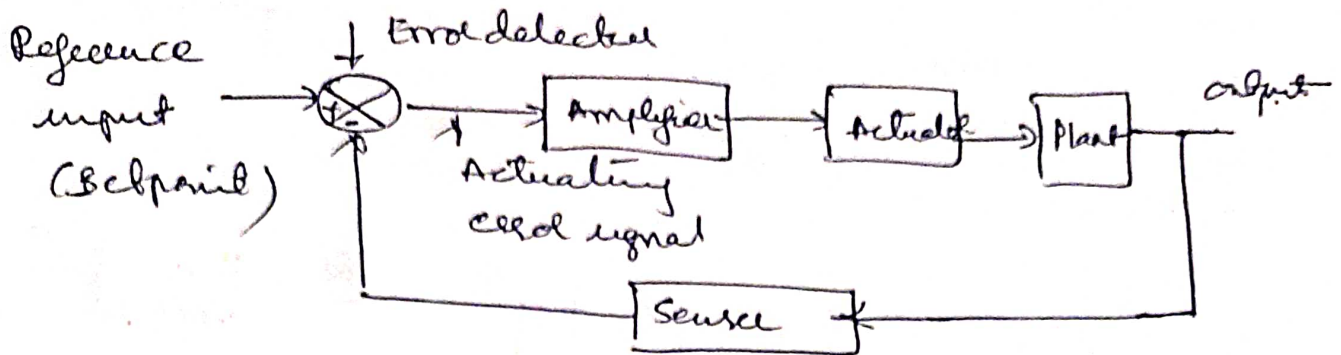
$$\text{Open loop transfer fun} = \frac{B(s)}{E(s)} = G(s) H(s)$$

$$\frac{H(s) C(s)}{R(s) - B(s)} = \frac{H(s) C(s)}{R(s) - E(s) G(s)} = \frac{H(s) \cancel{E(s)} G(s)}{\cancel{E(s)}} = H(s) G(s)$$

$B(s)$ = feedback signal $E(s)$ actuating error signal

Block diagram of an industrial control system is as follows.

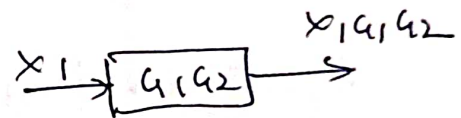
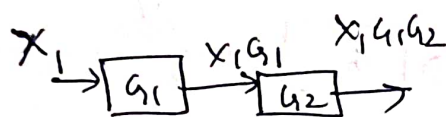
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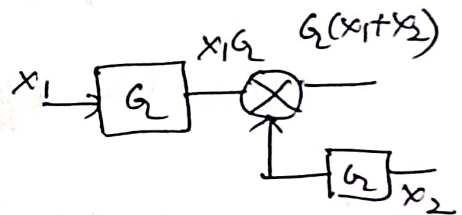
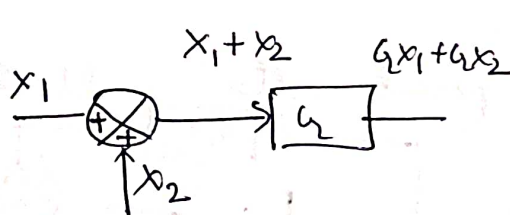
Rules of Block diagram algebra.

Rule original diagram Equivalent diagram

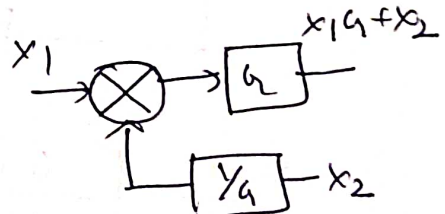
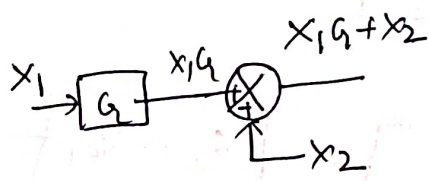
1) Combining blocks in cascade



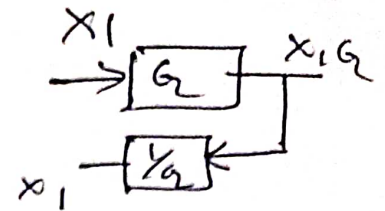
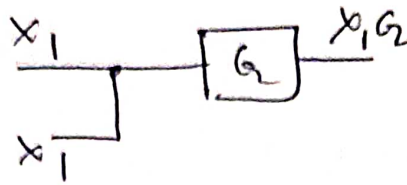
2) Moving summing point after a block



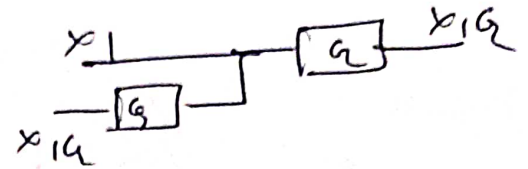
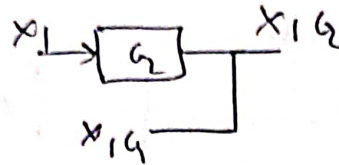
3) Moving summing point ahead of block



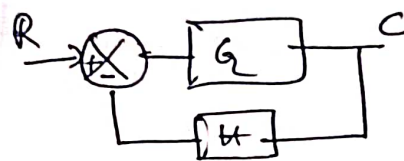
4) Moving a take off point after a block



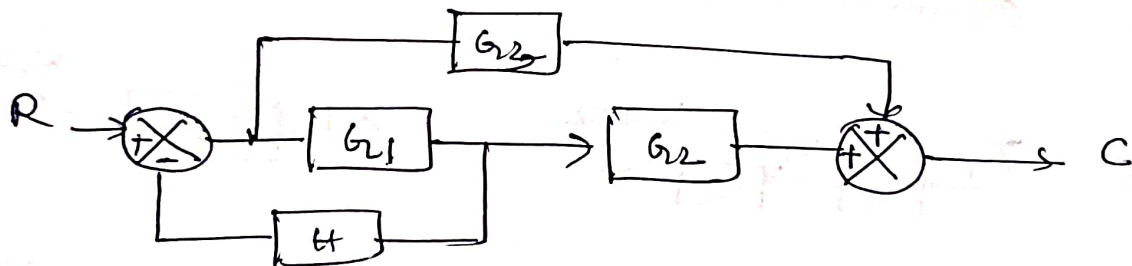
5) Moving a take off point ahead of block



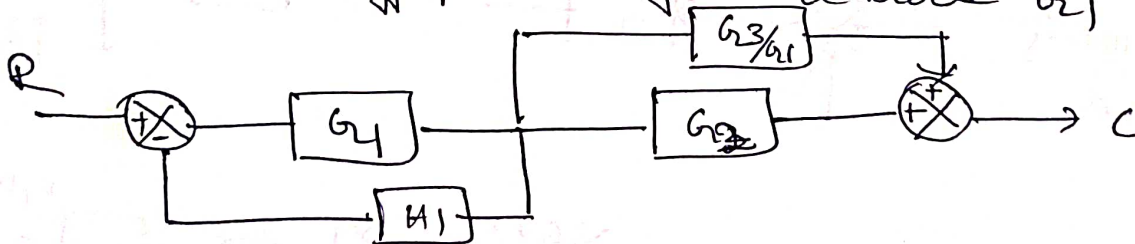
6) Eliminating a feedback loop



Eg. Reduce the block diagram shown & find C/R



Move take off point after a block G_1

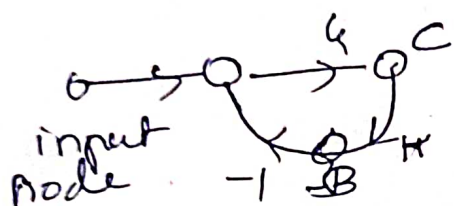


$$\therefore C/R = \frac{G_1 (G_2 + G_3/G_1)}{1 + G_1 H_1}$$

$$\frac{G_1 G_2 + G_3}{1 + G_1 H_1}$$

Signal flow graph

Block diagrams are very successful for representing control systems but for complicated systems the block diagram reduction process is tedious & time consuming. An alternate approach is that of signal flow graphs developed by S.J. Mason, which does not require any reduction process because of availability of a flow graph gain formula, which relates input & output system variables.



Mason's gain formula

The relationship between an input variable and an output variable of a signal flow graph is given by the net gain between the input and output nodes and is known as overall gain of the system.

$$T = \frac{1}{\Delta} \sum_k P_k \Delta_k$$

P_k = path gain of k^{th} forward path

Δ = determinant of the graph

$\Delta = 1 - (\text{sum of loop gains of individual loops}) + (\text{sum of gain product of all possible combination of two non-touching loops}) - \dots$

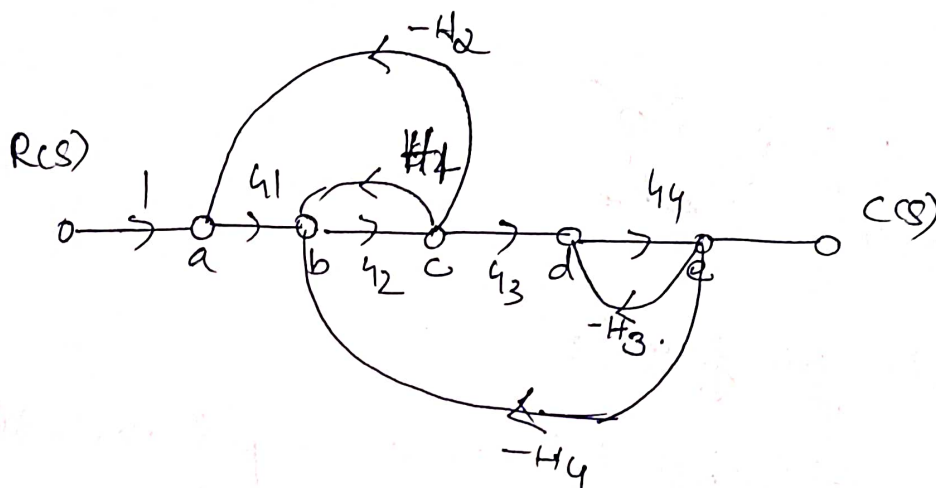
$$\Delta = 1 - \sum_m P_m + \sum_m P_m - \sum_m P_m g^+ - \dots$$

P_{mr} = gain product with possible combination of r non-touching loops

Δ_k = the value of Δ for the part of graph not touching the k th forward path

T = overall gain of the sys.

Determine c/R using Mason's gain formula



forward path

$$P_1 = G_1 G_2 G_3 G_4$$

$$\text{loops } L_1 - a-b-c-a = -G_1 G_2 H_2$$

$$L_2 - b-c-b = -G_2 H_1$$

$$L_3 \rightarrow d-e-d = -G_4 H_3$$

$$L_4 \rightarrow b-c-d-e-b = -G_2 G_3 G_4 H_4$$

non-touching loops

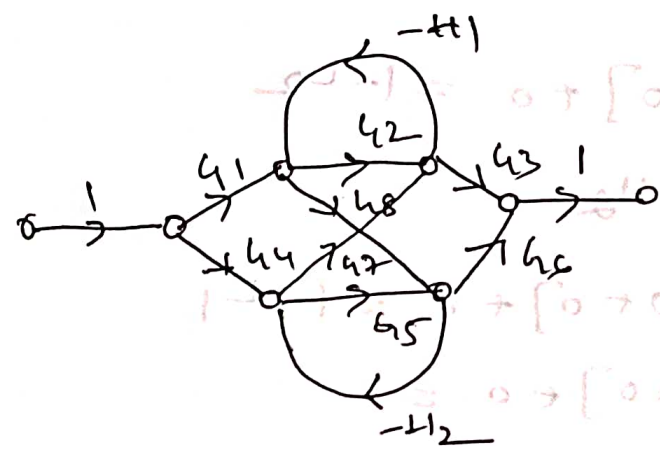
$$(-G_4 H_3) (-G_2 H_1) = G_2 G_4 H_1 H_3$$

$$-G_4 H_3 (-G_1 G_2 H_2) = G_1 G_2 G_4 H_2 H_3$$

$$T = \frac{P_1 \Delta_1 + P_2 \Delta_2 + P_3 \Delta_3 + P_4 \Delta_4}{\Delta}$$

$$T = \frac{G_1 G_2 G_3 G_4}{1 + G_1 G_2 H_2 + G_2 H_1 + G_4 H_3 + G_2 G_3 G_4 H_4 + G_1 G_2 G_4 H_2 H_3}$$

Find QR for the graph shown below using Mason's gain formula



$$T = \frac{\sum \Delta_k P_k}{\Delta}$$

① Forward path with gain

$$P_1 = G_1 G_2 G_3$$

$$P_2 = G_4 G_5 G_6$$

$$P_3 = G_1 G_8 G_6$$

$$P_4 = G_4 G_7 G_6$$

$$P_5 = G_1 G_8 - H_2 G_7 G_3$$

$$P_6 = G_4 G_6 - H_1 G_7 G_6$$

Individual loops

$$L_1 = -G_2 H_1 \quad L_2 = -G_5 H_2$$

$$L_3 = -H_1 G_8 - H_2 G_7 \\ = G_7 G_8 H_1 H_2$$

Two non-touching loops

$$L_1 L_2 = G_2 H_1 G_5 H_2$$

$$\Delta = 1 - [L_1 + L_2 + L_3] + L_1 L_2$$

$$\Delta_1 = 1 - [0 + L_2 + 0] + 0 = 1 - L_2 \\ = 1 + G_5 H_2$$

$$\Delta_2 = 1 - [L_1 + 0 + 0] + 0 = 1 - L_1$$

$$\Delta_3 = 1 - [0 + 0 + 0] + 0 = 1$$

$$\Delta_4 = 1$$

$$\Delta_5 = 1$$

$$\Delta_6 = 1$$

$$\frac{C(s)}{R(s)} = \frac{P_1 \Delta_1 + P_2 \Delta_2 + P_3 \Delta_3 + P_4 \Delta_4 + P_5 \Delta_5 + P_6 \Delta_6}{\Delta}$$

$$= \frac{G_1 G_2 G_3 (1 + G_5 H_2) + G_4 G_5 G_6 (1 + G_2 H_1) + G_1 G_8 G_6 \\ + G_4 G_7 G_3 - G_1 G_8 H_2 H_1 G_7 G_3 - G_4 G_7 H_1 G_8 G_6}{\Delta}$$

$$\Delta = 1 + G_2 H_1 + G_5 H_2 - H_1 G_8 H_2 G_7 + G_2 H_1 G_5 H_2$$

$$\therefore TF = \frac{G_1 G_2 G_3 (1 + G_5 H_2) + G_4 G_5 G_6 (1 + G_2 H_1) + G_1 G_8 G_6 \\ + G_4 G_7 G_3 - G_1 G_8 H_2 H_1 G_7 G_3 - G_4 G_7 H_1 G_8 G_6}{1 + G_2 H_1 + G_5 H_2 - H_1 G_8 H_2 G_7 + G_2 H_1 G_5 H_2}$$

Derive transfer function of a dc servomotor

In servo applications a motor is required to produce rapid accelerations from standstill.

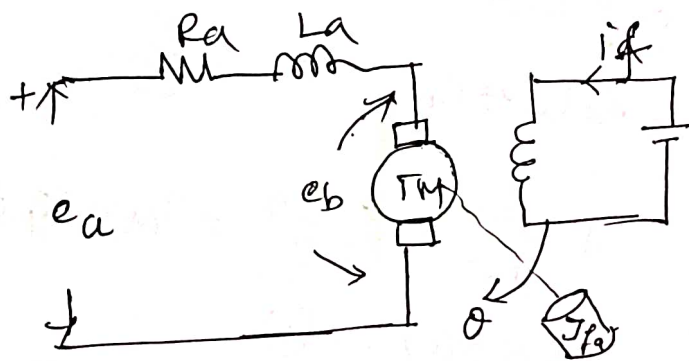
\therefore physical requirement of such motor are low inertia and high starting torque.

Armature control

Consider the armature controlled Dc motor

R_a = resistance of armature (Ω)

L_a inductance of armature winding (H)



i_a = armature current

i_f = field current

e_a = applied armature voltage

e_b = back emf

T_M = torque developed by motor shaft

J = Equivalent moment of inertia

f_0 = viscous friction coefficient of motor
or load to motor shaft (Nm/rad/s)

air gap flux

$$\phi = k_f i_f$$

$$\phi \propto i_f \text{ (field current)}$$

k_f constant

$$T_M = k_t k_f i_f i_a$$

k_t in a const

In armature controlled dc motor the field current is kept const.

$$T_M = k_T i_a$$

$$e_b = k_b \frac{d\theta}{dt} \rightarrow \text{back emf is proportional to speed}$$

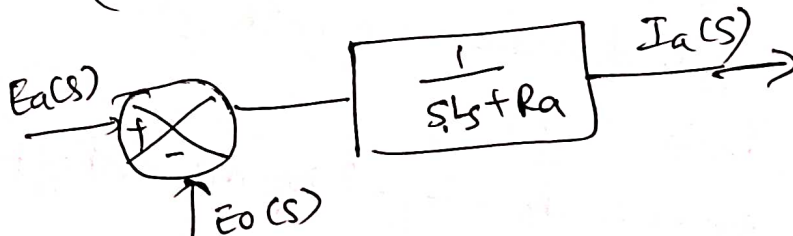
k_b - back emf const.

$$L_a \frac{di_a}{dt} + R_a i_a + e_b = e_a \quad \text{--- (1)}$$

Torque eqn $J \frac{d^2\theta}{dt^2} + f_0 \frac{d\theta}{dt} = T_M = K_t i_a$

$$E_b(s) = k_b s \theta(s) \quad \text{--- (b)}$$

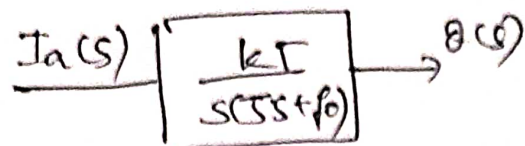
$$(L_s s + R_a) I_a(s) = E_a(s) - E_b(s) \quad \text{--- (2)}$$



②

$$(Js^2 + f_0 s) \theta(s) = T_M(s) = k_T I_a(s)$$

$$\theta(s) = \frac{k_T}{s(Js + f_0)} I_a(s)$$



T.F of the sys.

$$G(s) = \frac{\theta(s)}{E_a(s)} = \frac{k_T}{s [(R_a + sL_a) Js + f_0] + k_b k_s}$$

$$E_b(s) = k_b s \theta(s)$$

